

**Design of Mechanical Screw Jack for Mercedes E class**Akshay Shrishrimal¹, Pranav Patil², Ritesh Mane³¹, Dept. of Mechanical Engineering, MIT, Pune, India.², Dept. of Mechanical Engineering, MIT, Pune, India.³, Dept. of Mechanical Engineering, MIT, Pune, India.

Abstract: This paper analyzes the modification of the existing screw jack by incorporating an electric motor in the screw in order to make load lifting easier. In this modified design, the power screw is rotated through its connecting gear with the pinion gear which transmits its rotating speed to the pinion gear meshing with the bigger gear connected to the power screw to be rotated with required speed reduction and increased torque to drive the power screw. The significance and purpose of this work is to modify the existing car jack in order to make the operation easier, safer and more reliable in order to reduce health risks especially back ache problems associated with doing work in a bent or squatting position for a long period of time. The modified car jack is easy to use by pregnant women or whoever had problem with the vehicle tyre along the road. The designed jack will also save time and requires less human energy to operate. The design when adopted will effectively curb the problems associated with Ergonomics - which is a fundamental concept of design process. The Design a mechanical screw jack is for Mercedes e class having weight 1400kg and ground clearance 180mm.

Keywords- Jack, Power Screw, Ergonomic, Pinion Gear, Speed Reduction, Torque

I. INTRODUCTION

A screw jack is a portable device consisting of a screw mechanism used to raise or lower the load. There are two types of jack.

1. Hydraulic jack- A hydraulic jack consists of a cylinder and piston mechanism. The movement of the piston rod is used to raise or lower the load.
2. Mechanical jack- Mechanical jacks can be either hand operated or power driver. Although a jack is simple and widely used device, the use of any lifting device is subject to certain hazards. In screw jack application, the hazards are dropping tripping or slipping of machines or their parts.

1.1 Causes of failure

The load is improperly screwed on jack. The screw jack is overloaded the centre of gravity of load is off centre with respect to axis of the jack. The screw jack is not placed on hard and level surface. The screw jack is used for a purpose for which it is not designed.

Essential for a screw jack

Proper size, strength, stability are essential requirements for the design of the screw jack from safety consideration.

1.2 Selection of material

- I. Frame - The frame of the screw jack has complex shape. It is subjected to compressive stress. Grey cast iron of grade FG 200 ($S_{ut} = 200 \text{ N/mm}^2$) is selected as the material for the frame. Cast iron is cheap and it is given any complex shape without involving any costly machining operations.
- II. Screw - The screw is subjected to torsional moment, compressive force and bending moment. From strength consideration plain carbon steel of grade 30C8 ($S_{yt} = 400 \text{ N/mm}^2$ and $e = 207000 \text{ N/mm}^2$) is selected as material for the screw.

1.3 Design of screw jack parameters

Total force = 300 N

Weight $W = 3.4335 \text{ KN}$

FOS = 2.5

$S_{yc} = S_{yt} = 560 \text{ MPA}$

$$\sigma_c = \frac{S_{yc}}{FOS} = 224 \text{ MPA}$$

1.3.1. Core diameter

$$\sigma = \frac{W}{\frac{\pi}{4}(dc)^2}$$

$$dc = 6.2476 \text{ mm}$$

1.3.2 For torsional

Let $d_c = 12 \text{ mm}$
 Nominal diameter = 16 mm
 Pitch = 4 mm
 $d = 16 \text{ mm}$
 $P = 4 \text{ mm}$

$$d_m = d - 0.5 p$$

$$= 16 - 0.5 \times 4 = 14 \text{ mm}$$

For single start
 $P = 4 \text{ mm}$

$$\tan \alpha = \frac{1}{\pi \times dm}$$

$$\alpha = 5.196^\circ$$

Let $\mu = 0.2$
 Talking into account bad lubrication and operating condition

$$\tan \phi = \mu$$

$$\phi = 63.43^\circ$$

$\phi > \alpha$
 $63.43 > 5.196$
 Screw is self-locking

$$T = W \times \frac{dm}{2} \times \tan(\phi + \alpha)$$

$$T = 61.41 \times 10^3 \text{ Nmm}$$

1.3.3 At section xx

$$\tau_{max} = \frac{16 T}{\pi * dc^3}$$

$$\tau_{max} = 0.18 \text{ MPA}$$

$$\tau_{permissible} = \frac{0.5 Syt}{FOS}$$

$$\tau_{permissible} = 112 \text{ MPA}$$

$112 \text{ MPA} > 0.18 \text{ MPA}$
 Hence, Screw is safe in tension

1.3.4 Stress due to bending

$M_b = P \times L$
 $L = 100 \text{ mm}$
 $M_b = 30 \text{ Nm}$

$$\sigma_{bending} = \frac{32 mb}{\pi * dc^3}$$

$$\sigma_{bending} = 176.83 \text{ MPA}$$

$$224 \text{ MPA} > 176.83 \text{ MPA}$$

Hence, Screw is safe in bending

$$\tau_{\max} = \sqrt{\left(\frac{\sigma_b}{2}\right)^2 + \tau^2}$$

$$\tau_{\max} = 86.41 \text{ MPA}$$

$$86.41 \text{ MPA} < 112 \text{ MPA}$$

Hence, Screw is safe in combined torsional and bending moment.

End fixity co-efficient (n) is 0.25

$$\frac{S_{yt}}{2} = \frac{n \times \pi^2 \times E}{\left(\frac{L}{K}\right)^2}$$

$$\frac{I}{K} = 42.709$$

We consider length as 100 mm

$$K = \sqrt{\frac{I}{K}}$$

I = moment of inertia

K= radius of gyration

$$I = \frac{\pi}{4} \times dc^4$$

$$I = 16286.016 \text{ mm}^2$$

$$A = 113.097 \text{ mm}^2$$

$$K = 12$$

$$\text{Slenderness ratio} = \frac{L}{K} = \frac{100}{11.5} = 8.333$$

$$P_{cr} = \frac{\pi^2 EI}{\left(\frac{L}{K}\right)^2}$$

$$P_{cr} = 4560 \text{ KN} > 75 \text{ KN}$$

Bearing pressure between steel screw and bronze nut is 10 MPa

$$P_b = W \left(\frac{\pi}{4} (do^2 - dc^2) Z \right)$$

$$Z = 4$$

$$\text{Height (H)} = 4 \times 4 = 16 \text{ mm}$$

1.3.5 Transverse shear stress

$$\tau = \frac{W}{\pi d T Z}$$

$$\tau = 8.5384 \text{ MPa}$$

$$8.5384 < 14 \text{ MPa}$$

Hence, Nut is safe

1.3.6 Transverse shear stress in threads

$$\text{Transverse shear stress} = \frac{3433.5}{\pi \times 12 \times 2 \times 4}$$

$$= 11.38 \text{ MPa} < 12 \text{ MPa}$$

It is safe for the transverse shear stress

1.3.7 Nut design for cross-section

$$\sigma_t = \frac{W}{\frac{\pi}{4}(D_o^2 - D_i^2)}$$

$$D_o = 16.008 \text{ mm}$$

By using empirical relations
 $D_o = 1.6(16.008)$
 $D_o = 20.8 \text{ mm}$

1.3.8. For width column

$$\tau = \frac{W}{\pi \times D_o \times t}$$

$$t = 3.5933 \text{ mm}$$

$$\sigma_c = W / \left(\frac{\pi}{4} (D_o^2 - D_c^2) \right)$$

$$\sigma_c = 24.78 \text{ Mpa}$$

$$= 24.78 \text{ Mpa} < 38 \text{ MPa}$$

1.3.9. Design of cup

$$D = 1.6 \times d$$

$$D = 25.6 \text{ mm}$$

$$D^1 = 0.8 d$$

$$D^1 = 12.8 \text{ mm}$$

1.3.10. Collar friction

$$T_f = \frac{\mu W}{4} (D_o - D_i)$$

$$T_f = 22661.1 \text{ Nmm}$$

Therefore, Total torque = $T_f + T = 84071 \text{ Nmm}$
 This torque operator has to be overcome

$$84071 = 300 \times 0.9 \times 2 \times L_h$$

$$L_h = 155.687 \text{ mm}$$

The length of handle 155.69 mm is practically possible, so no need of thrust ball bearing, length of handle is assumed to be 180 mm.

$$M_h = F \times L_c$$

$$= 54000 \text{ Nmm}$$

Hence the design is safe.

II. MANUFACTURING METHODS OF SCREW JACK

1. Frame –Gray cast iron of grade FG 200 is selected as the material for the frame. It is technically and economically advantageous to use cast iron for the frame. The frame is mainly manufactured by casting process as it is easier to manufacture complex shapes using casting.
2. Lead screw-For strength consideration plain carbon steel of grade 30c8 is selected as material. It is manufactured by rolling process, metal stock is passed through one or more pairs of rolls to reduce the thickness and to make the thickness uniform.
3. Nut –Since wear occurs between the screw and the nut, it is always desirable that the wear takes place in the nut, so that the nut is replaced. Hence it is made of a softer material cast of phosphor bronze of grade -1. It is selected as the material for the nut. Nut is manufactured by the casting process. Casting process is versatile and light and complex component can be manufactured using casting.
4. Cup –Grey cast iron grade FG 200 is used for the cup. The shape and dimensions of the cup are such that it is easier and economical to make it by casting process.
5. Handle –The yield strength is the criterion for the selection of material. Plain carbon steel of grade 30c8 is selected as material for the handle. It is manufactured by casting process.

III. CONCLUSION

1. Self-locking of the screw is not possible when the coefficient of friction (μ) is low. The coefficient of friction between the surfaces of the screw and the nut is reduced by lubrication. Excessive lubrication may cause the load to descend on its own.
2. The self-locking property of the screw is lost when the lead is large. The lead increases with number of starts. For double-start thread, lead is twice of the pitch and for triple threaded screw, three times of pitch. Therefore, the single threaded screw is better than multiple threaded screws from self-locking considerations.

IV. RECOMMENDATION

1. Further research should be carried out on how to minimize vibration and noise during operation.
2. Design applicable to vehicles weighing over 1000 kg should be carried out

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